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(54) Resonator cavity end wall assembly

(57) An electromagnetic resonator (10) comprises a waveguide body (12) having a generally tubular side wall (14) and a pair of end wall assemblies (18). The end wall assembly (18) includes a bowed aluminum plate (22) and an INVAR disk (24), attached to one another at the periphery thereof. The INVAR disk (24) includes a relatively thick outer annular portion (30) and a relatively thin inner circular portion (32). The bowed aluminum plate (22) bows in response to increased temperature, thereby counteracting expansion of the waveguide body (12).

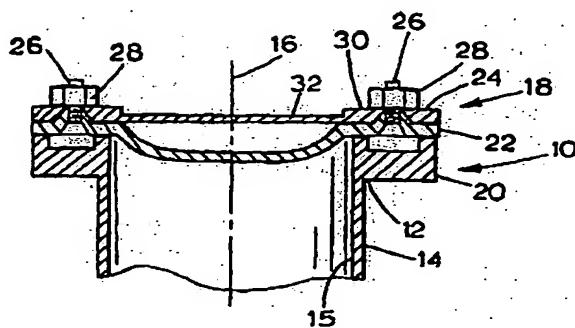


FIG. 1

Description**BACKGROUND OF THE INVENTION****(a) Field of the Invention**

[0001] This invention relates to thermal stabilization of a single cavity structure, or a multiple cavity structure (wherein cylindrical cavities are arranged coaxially in tandem, as in the construction of a microwave filter of plural resonant chambers, or cavities), and, more particularly, to an arrangement of one or more cavities employing at least one transverse bowed end wall including materials with differing coefficients of thermal expansion to provide selected ratios of thermally induced deformation of the end wall to counteract changes in resonance induced by thermal expansion/contraction of an outer cylindrical wall of the cavity structure.

(b) Description of Related Art

[0002] Cavity structures are employed for microwave filters. As is known in the art, a cavity resonator is, in effect, a tuned circuit which is utilized to filter electromagnetic signals of unwanted frequencies from input electromagnetic energy and to output signals having a preselected bandwidth centered about one or more resonant frequencies. A cavity which is frequently employed for a cavity resonator has the shape of a right circular cylinder wherein the diameter and the height (or the axial length) of the cavity together determine the value of a resonant frequency. For filters described mathematically as multiple pole filters, it is common practice to provide a cylindrical housing with transverse disc shaped partitions or walls defining the individual cavities. Irises in the partitions provide for coupling of desired modes of electromagnetic waves between the cavities to provide a desired filter function or response.

[0003] A problem arises in that changes in environmental temperature induce changes in the dimensions of the filter with a consequent shift in the resonant frequency of each filter section. Because the resonant frequency associated with each cavity is a function of the cavity's dimensions, an increase in temperature will cause dimensional changes in the cavity and, therefore, temperature-induced changes in the resonant frequency associated with the cavity. Specifically, an increasing temperature will cause thermal expansion of the waveguide body to enlarge the cavity both axially and transversely.

[0004] A filter fabricated of aluminum undergoes substantial dimensional changes as compared to a filter constructed of invar nickel-steel alloy (herein referred to as "INVAR") due to the much larger thermal coefficient of expansion for aluminum as compared to INVAR. However, it is often the case that aluminum is nevertheless a preferable material for constructing filters, espe-

cially for aerospace applications, due to its lower density, as well as its greater ability to dissipate heat, as compared to that of INVAR.

[0005] A solution to the foregoing problem, useful especially for a two-cavity filter, is presented in U.S. Pat. No. 4,677,403 of Kich (hereinafter, "the '403 patent"), the entirety of which is hereby incorporated by reference. Therein, an end wall of each cavity is formed of a bowed disc, while a central wall having an iris for coupling electromagnetic energy has a planar form. An increase of temperature enlarges the diameter of each cavity, and also increases the bowing of the end walls, with a consequent reduction in the axial length of each cavity. The resonant frequency shift associated with the increased diameter is counterbalanced by the shift associated with the decrease in length. Similar compensation occurs during a reduction in temperature wherein the diameter decreases and the length increases.

[0006] Another approach is presented in U.S. Pat. No. 5,374,911 of Kich et al. (hereinafter, "the '911 patent"), the entirety of which is hereby incorporated by reference, and which, discloses a cylindrical filter structure of multiple cavities with a succession of transverse walls defining the cavities. Selected ones of the transverse walls provide for thermal compensation. Each of the selected transverse walls is fabricated of a bowed disc encircled by a ring formed of material of lower thermal expansion coefficient than the material of the transverse wall. Inner ones of the transverse walls are provided with irises for coupling electromagnetic power between successive ones of the cavities. By varying the composition of the rings to attain differing coefficients of thermal expansion within the rings, different amounts of bowing occur in the corresponding transverse discs with changes in temperature. Thus, the ring of an inner transverse wall has a relatively large coefficient of thermal expansion as compared to the ring of an outer one of the transverse walls, resulting in a lesser amount of bowing of the inner wall and a larger amount of bowing of the outer wall with increase in environmental temperature and temperature of the filter.

[0007] In a preferred embodiment disclosed in the '911 patent, the housing is constructed of aluminum, as is a central planar transverse wall having a coupling iris. The other transverse walls, both to the right and to the left of the central wall, are provided with a bowed structure, the bowed walls being encircled by metallic rings. The inboard rings nearest the central wall are fabricated of titanium, and the outboard rings are fabricated of INVAR. The INVAR has a lower coefficient of thermal expansion than does the titanium and, accordingly, the peripheral portions of the outboard walls, in the case of a four-cavity structure, experience a more pronounced bowing upon a increase in environmental temperature than do the inner walls which are bounded by the titanium rings having a larger coefficient of thermal expansion.

[0008] The reason for the use of the rings of differing

coefficients of thermal expansion is as follows. Deflection of an inboard wall reduces the axial length of an inner cavity, on the inner side of the wall, while increasing the dial length of an outer cavity, on the opposite side of the wall, with increasing temperature. Thus, the inboard wall acts in the correct sense to stabilize the inner cavity but in the incorrect sense for stabilization of the outer cavity. Accordingly, in stabilizing the outer cavity by means of the outer wall, it is necessary to provide an additional bowing to overcome the movement of the inboard wall, to thereby stabilize thermally the outer cavity.

[0009] One disadvantage associated with a resonator structure constructed in accordance with either the '403 patent or the '911 patent is that the relatively thin aluminum disk used for the end wall, that is capable of bowing in response to increased temperature, has a tendency to exhibit undesirable thermal gradients across the surface of the end wall, resulting in a frequency shift when RF power is applied.

[0010] Accordingly, there is a need for an electromagnetic resonator end wall assembly configured so as to minimize or eliminate the aforementioned problems.

SUMMARY OF THE INVENTION

[0011] In accordance with one aspect of the present invention, an end wall assembly for an electromagnetic filter comprises a first plate made from a material having a first coefficient of thermal expansion, and a second plate attached to the first plate and made from a material having a second coefficient of thermal expansion substantially less than the first coefficient of thermal expansion.

[0012] Preferably, the first plate is made from aluminum and the second plate is made from INVAR. The second plate is preferably bolted or otherwise attached to the periphery of the first plate.

[0013] In accordance with another aspect of the present invention, an electromagnetic filter comprises a resonator having a housing, including an end wall assembly. The housing defines a substantially cylindrical cavity and the end wall assembly includes a first plate adjacent to the cylindrical cavity and made from a material having a first coefficient of thermal expansion. The end wall assembly further includes a second plate attached to the first plate, the second plate having a second coefficient of thermal expansion substantially less than the first coefficient of thermal expansion.

[0014] In accordance with still another aspect of the present invention, an electromagnetic filter comprises a resonator having a housing, including an end wall assembly, the housing defining a substantially cylindrical cavity. The end wall assembly includes a first plate adjacent to the cylindrical cavity, having a periphery, and made from a material having a first coefficient of thermal expansion. The end wall assembly further includes a second plate attached to the periphery of the

first plate, the second plate having a second coefficient of thermal expansion substantially less than the first coefficient of thermal expansion. The periphery of the first plate is substantially constrained from radial expansion in response to elevated temperature, the first plate is adapted to bow away from the second plate in response to elevated temperature, and the first and second plates are adapted to bend in response to elevated temperature, due to a bimetallic effect.

[0015] A resonator in accordance with the present invention has optimal thermal stability, while permitting the use of thicker aluminum plates for the end wall assembly, thereby reducing the severity of thermal gradients across the surface of the end wall assembly, and reducing resultant frequency shifts when RF power is applied.

[0016] The invention itself, together with further objects and attendant advantages, will best be understood by reference to the following detailed description, taken in conjunction with the accompanying drawings.

BRIEF DESCRIPTION OF THE DRAWINGS

[0017]

FIG. 1 is a longitudinal, fragmentary cross-sectional view of a cavity resonator with an end wall assembly in accordance with the present invention;

FIG. 2 is a plan view of the end wall assembly of FIG. 1;

FIG. 3 is a bottom view of the end wall assembly of FIG. 1; and

FIG. 4 is a cross-sectional view, similar to that of FIG. 1, showing the end wall assembly at an elevated temperature.

DESCRIPTION OF THE PREFERRED EMBODIMENTS

[0018] FIG. 1 illustrates a preferred embodiment of a cavity resonator or filter, generally indicated at 10, constructed in accordance with the present invention. The resonator 10 comprises a waveguide body 12, preferably made from aluminum and having a generally tubular sidewall 14 generally disposed about a central axis 16, and a pair of end wall assemblies, one of which is indicated generally at 18. The generally tubular sidewall 14 of the waveguide body 12 defines a substantially circular cylindrical cavity 15. The waveguide body 12 includes a flange portion 20 at either end thereof. The end wall assembly 18 is secured to the waveguide body 12 by any suitable means, such as, for example, by securing the end wall assembly 18 to the flange portion 20 using screws (not shown).

[0019] The end wall assembly 18 includes a first plate in the form of a bowed aluminum plate 22 and a second plate in the form of an INVAR disk 24. The INVAR disk 24 includes an outer annular portion 30 that is relatively

thick, and an inner circular portion 32 that is relatively thin. The bowed aluminum plate 22 is attached at the periphery thereof to the outer annular portion 30 of the INVAR disk 24 by means of bolts 26 and nuts 28. Attachment of the bowed aluminum plate 22 to the outer annular portion 30 of the INVAR disk 24 can be accomplished alternatively by way of diffusion bonding, eutectic soldering/brazing, friction welding or welding, by way of example.

[0020] The configuration of the end wall assembly 18 at an elevated temperature is shown in FIG. 4. The bowed aluminum plate 22 has a coefficient of thermal expansion which is higher (by a multiplicative factor of about ten) than the coefficient of thermal expansion of the INVAR disk 24. As a result of the attachment of the periphery of the bowed aluminum plate 22 to the outer annular portion 30 of the INVAR disk 24, the peripheral region of the bowed aluminum plate 22 is allowed to expand only slightly with increasing environmental temperature, while the central portion of the bowed aluminum plate 22 is free to expand with a resultant increased bowing of the bowed aluminum plate 22 due to an "oil can" effect. This increased bowing of the bowed aluminum plate 22 is enhanced by the ability of the INVAR disk 24 to also bend due to a thermally-induced bending moment resulting from the difference in the coefficients of thermal expansion as between the INVAR disk 24 and the bowed aluminum plate 22 (i.e., bimetallic effect).

[0021] Because of this enhanced bowing of the bowed aluminum plate 22, the bowed aluminum plate 22 can have a greater thickness (i.e., increased by approximately 100%), as compared to the thickness that would be required if the bowed aluminum plate 22 were attached to an INVAR or titanium ring (as in the Kich et al. '911 patent), thus reducing the severity of thermal gradients across the surface of the end wall assembly, and reducing resultant frequency shifts when RF power is applied. The resonator 10 constructed in accordance with the present invention can maintain an overall effective coefficient of thermal expansion for the cavity 15 that is approximately one-third of that of a resonator made entirely of INVAR.

[0022] The reverse effect, with reduced bowing of the bowed aluminum plate 22, occurs upon a reduction in the environmental temperature. Although the outer annular portion 30 of the INVAR disk 24 is thicker than the inner circular portion 32, the outer annular portion 30 is substantially thinner than the INVAR ring disclosed in the Kich et al. '911 patent.

[0023] Cavity resonators employing two or more cavities are well known and are within the purview of the invention. Such resonators employ the appropriate number of coupling irises to effectively divide the housing interior into the desired number of appropriately dimensioned cavities.

[0024] While the present invention has been described with reference to specific examples, which

are intended to be illustrative only, and not to be limiting of the invention, it will be apparent to those of ordinary skill in the art that changes, additions and/or deletions may be made to the disclosed embodiments without departing from the scope of the invention as defined by the appended claims. For example, the shape of the cavity 15 can be rectangular or elliptical in cross-section, rather than circular, without departing from the scope of the invention as defined by the appended claims.

Claims

1. An end wall assembly (18) for an electromagnetic filter (10) having a waveguide body (12), the end wall assembly (18) comprising:
 - 15 a first plate (22) made from a material having a first coefficient of thermal expansion and being secured to the waveguide body (12); and means (24) for thermal compensation of the characteristic of the filter (10); characterized in that said compensation means (24) is a second plate (24) directly attached to the first plate (22) and made from a material having a second coefficient of thermal expansion substantially less than the first coefficient of thermal expansion.
 - 20 2. The end wall assembly (18) of claim 1, characterized in that the first plate (22) is made from aluminum.
 - 25 3. The end wall assembly (18) of claim 1 or claim 2, characterized in that the second plate (24) is made from INVAR.
 - 30 4. The end wall assembly (18) of any of claims 1 through 3, characterized in that the second plate (24) is attached, particularly bolted to the periphery of the first plate (22).
 - 35 5. The end wall assembly (18) of any of claims 1 through 4, characterized in that the first plate (22) is bowed away from the second plate (24).
 - 40 6. The end wall assembly (18) of any of claims 1 through 5, characterized in that said second plate (24) is a continuous plate.
 - 45 7. The end wall assembly (18) of any of claims 1 through 6, characterized in that the second plate (24) includes an outer annular portion (30) that is relatively thick, and an inner circular portion (32) that is relatively thin.
 - 50 8. The end wall assembly (18) of any of claims 1
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through 7, characterized in that said first plate (22) and said second plate (24) are secured to the waveguide body (12).

9. The end wall assembly of any of claims 1 through 8, characterized in that the first plate (22) has a periphery, that the second plate (24) is attached to the periphery of the first plate, and that the periphery of the first plate (22) is substantially constrained from radial expansion in response to elevated temperature due to the attachment of the second plate (24) to the periphery of the first plate (22), the first plate (22) is adapted to bow away from the second plate (24) in response to elevated temperatures, and the first and second plates (22, 24) are adapted to bend in response to elevated temperatures. 5
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10. An electromagnetic filter (10) comprising:

a resonator (10) having a housing (12), the housing (12) defining a substantially cylindrical cavity (15), and an end wall assembly (18) adjacent to the cylindrical cavity (15), characterized in that the end wall assembly (18) is an end wall assembly according to any of claims 1 20
25 through 9.

11. The electromagnetic filter (10) of claim 10, characterized in that the cavity (15) is a substantially circular cylindrical cavity (15). 30

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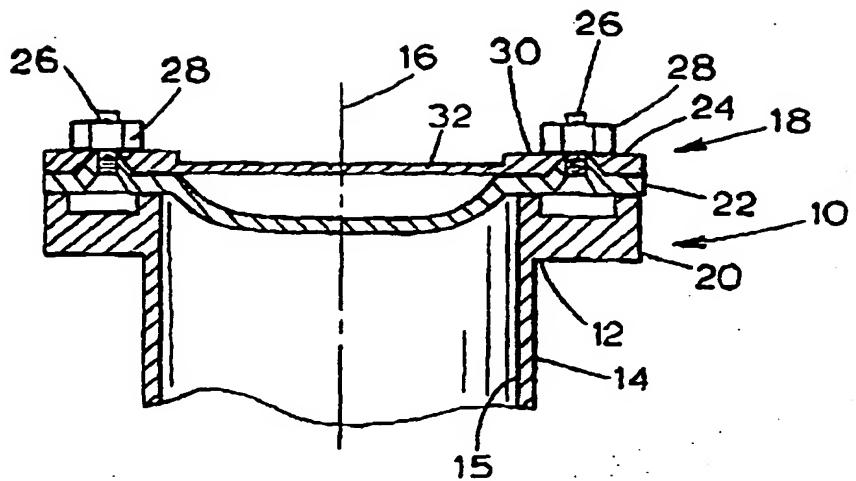


FIG. 1

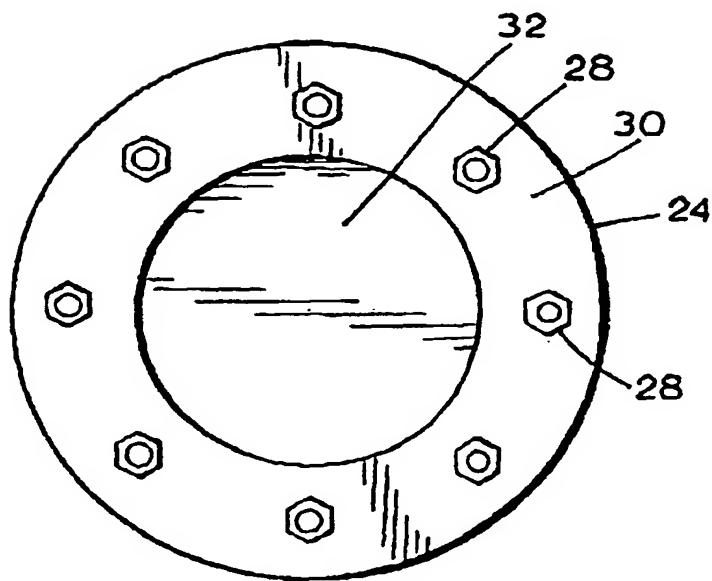


FIG. 2

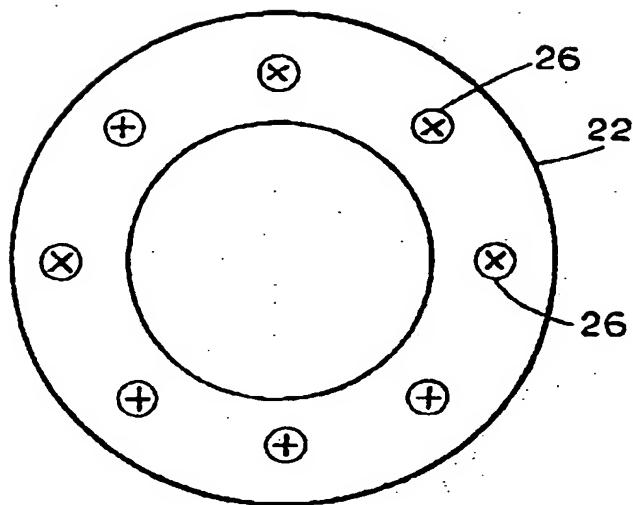


FIG. 3

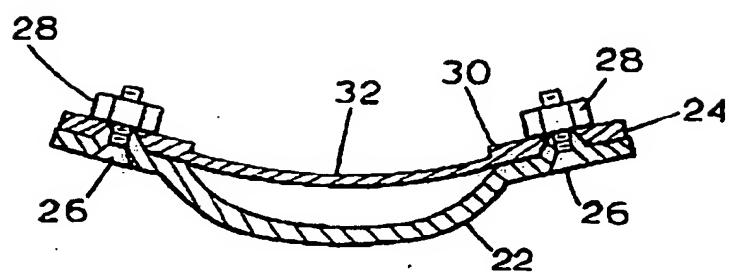


FIG. 4



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EUROPEAN SEARCH REPORT

Application Number

EP 99 10 2786

DOCUMENTS CONSIDERED TO BE RELEVANT									
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.6)						
X	WO 87 03745 A (HUGHES AIRCRAFT COMPANY) 18 June 1987 * page 4, line 24 - page 9, line 26; figure 1 *	1, 3-6, 8-11	H01P7/06						
Y	---	2, 7							
Y	EP 0 540 360 A (LK-PRODUCTS OY) 5 May 1993 * column 3, line 49 - column 6, line 5; figures 1, 4 *	2							
Y	US 4 059 815 A (MAKIMOTO ET AL.) 22 November 1977 * column 4, line 30 - column 5, line 53; figure 4 *	7							
A	FR 1 006 613 A (ONERA) 3 May 1952 * page 2, right-hand column, line 44 - line 49; figure 4 *	1							
TECHNICAL FIELDS SEARCHED (Int.Cl.6)									
H01P									
<p>The present search report has been drawn up for all claims</p> <table border="1" style="width: 100%; border-collapse: collapse;"> <tr> <td style="width: 33%;">Place of search</td> <td style="width: 33%;">Date of completion of the search</td> <td style="width: 33%;">Examiner</td> </tr> <tr> <td>THE HAGUE</td> <td>20 May 1999</td> <td>Den Otter, A</td> </tr> </table>				Place of search	Date of completion of the search	Examiner	THE HAGUE	20 May 1999	Den Otter, A
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THE HAGUE	20 May 1999	Den Otter, A							
CATEGORY OF CITED DOCUMENTS		T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document							
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**ANNEX TO THE EUROPEAN SEARCH REPORT
ON EUROPEAN PATENT APPLICATION NO.**

EP 99 10 2786

This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

20-05-1999

Patent document cited in search report		Publication date		Patent family member(s)		Publication date
WO 8703745	A	18-06-1987		US 4677403 A CA 1257349 A DE 3682905 A EP 0253849 A JP 6050804 B		30-06-1987 11-07-1989 23-01-1992 27-01-1988 29-06-1994
EP 0540360	A	05-05-1993		FI 915156 A DE 69209223 D DE 69209223 T DK 540360 T JP 5235620 A US 5304968 A		01-05-1993 25-04-1996 14-08-1996 15-04-1996 10-09-1993 19-04-1994
US 4059815	A	22-11-1977		JP 1303213 C JP 52017748 A JP 60012801 B JP 1316576 C JP 52017749 A JP 60034281 B CA 1080313 A		28-02-1986 09-02-1977 03-04-1985 15-05-1986 09-02-1977 08-08-1985 24-06-1980
FR 1006613	A	03-05-1952		NONE		

For more details about this annex : see Official Journal of the European Patent Office, No. 12/82